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- 3D Structure and motion
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3D structure and motion: Approaches

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 - Finite displacement-based
- Seek to recover
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 - 3D structure (geometric layout of environment)

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Where we will go

- We now will develop an approach to recovering 3D structure and motion.
- Here, we will assume
 - arbitrary 3D motion
 - orthographic model of image formation
 - as input we have extracted the position n image points, corresponding to scene points $P_1, P_2, ..., P_n$, not all coplanar, and they have been tracked across $N \ge 3$ frames, For example, the points tracks might be acquired from the feature-based, finite displacement algorithm described earlier as it operates across an entire video sequence.
- The overall approach is known as the factorization approach, as it relies on a clever observation about how we can factor matrices of feature correspondences into 2 matrices.
 - One matrix captures the 3D structure.
 - The other matrix captures the 3D motion.

Notation

• Let

$$\boldsymbol{p}_{ij} = (x_{ij}, y_{ij})^{\mathrm{T}}$$

denote the *j*th image point (j = 1, ..., n) at the *i*th frame, (i=1, ..., N).

• Think of the *xij* and *yij* as entries of two $N \ge n$ matrices **X** and **Y**.

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• Now, subtract the mean of the entries on the same row from each xij and yij

$$\overline{x}_{ij} = x_{ij} - \overline{x}_i \qquad \overline{y}_{ij} = y_{ij} - \overline{y}_i$$

where

$$\overline{x}_i = \frac{1}{n} \sum_{j=1}^n x_{ij} \qquad \overline{y}_i = \frac{1}{n} \sum_{j=1}^n y_{ij}$$

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 Now stack these registered points analogously to our previous construction to form the registered measurement matrix

$$\overline{\mathbf{W}} = \begin{bmatrix} \mathbf{X} \\ \overline{\mathbf{Y}} \end{bmatrix}$$

The rank theorem (statement)

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- The proof is based on a decomposition (factorization) of the matrix in the product of a 2*N* x 3 matrix, **R**, and a 3 x *n* matrix **S**.
- **R** describes the frame-to-frame motion (rotation) of the camera with respect to the points P_j .
- **S** describes the 3D structure (or shape) of the points.

The rank theorem (proof)

$$\frac{1}{n}\sum_{j=1}^{n}\boldsymbol{P}_{j}=0$$



The rank theorem (proof)

• Consider all quantities expressed in an object-centred reference frame with the origin at the centroid of *P*₁, ..., *P*_n. Thus,

$$\frac{1}{n}\sum_{j=1}^{n}\boldsymbol{P}_{j}=0$$

• Let **i***i* and **j***i* denote the unit vectors that define the image reference frame, expressed in the world reference frame at time *i*.



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- Let *T*, be the vector from the world origin to the origin of the *i*th image frame.
- We have $x_{ij} = \mathbf{i}_i^{\mathbf{T}} (\mathbf{P}_j \mathbf{T}_i)$ $y_{ij} = \mathbf{j}_i^{\mathbf{T}} (\mathbf{P}_j \mathbf{T}_i)$



The rank theorem (proof)

• Now, the registered points can be written as

$$\overline{x}_{ij} = \mathbf{i}_i^{\mathrm{T}} (\boldsymbol{P}_j - \boldsymbol{T}_i) - \frac{1}{n} \sum_{m=1}^n \mathbf{i}_i^{\mathrm{T}} (\boldsymbol{P}_m - \boldsymbol{T}_i)$$
$$\overline{y}_{ij} = \mathbf{j}_i^{\mathrm{T}} (\boldsymbol{P}_j - \boldsymbol{T}_i) - \frac{1}{n} \sum_{m=1}^n \mathbf{j}_i^{\mathrm{T}} (\boldsymbol{P}_m - \boldsymbol{T}_i)$$

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and the fact that the index i is not summed, we have

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• So, we define

$$\mathbf{R} = \begin{bmatrix} \mathbf{i}_{1}^{\mathbf{T}} \\ \vdots \\ \mathbf{i}_{N}^{\mathbf{T}} \\ \mathbf{j}_{1}^{\mathbf{T}} \\ \vdots \\ \mathbf{j}_{N}^{\mathbf{T}} \end{bmatrix} \qquad \mathbf{S} = \begin{bmatrix} \mathbf{P}_{1} & \mathbf{P}_{2} & \cdots & \mathbf{P}_{n} \end{bmatrix}$$

• And write $\overline{\mathbf{W}} = \mathbf{RS}$

The rank theorem (proof)

• Finally, we note that given the constructions

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R is $2N \ge 3$ of rank 3, because $N \ge 3$; further, **S** is $3 \ge n$ and also is of rank 3, because the *n* points in 3D space are not all coplanar.

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The factorization algorithm

• Factorization of the (registered) measurement matrix can be accomplished via application of the SVD (recall Unit 5 interlude), i.e.,

$$\overline{\mathbf{W}} = \mathbf{U}\mathbf{D}\mathbf{V}^{\mathrm{T}}$$

• Here, for $\overline{\mathbf{W}}$ having dimensions $2N \ge n$, \mathbf{U} is $2N \ge 2N$, \mathbf{V} is $n \ge n$ and \mathbf{D} is $2N \ge n$.

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- Let
 - **D**' be the 3 x 3 top left submatrix of **D** corresponding to its 3 largest singular values.
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• But, we are not quite done ...

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 Indeed, the SVD factorization is not unique: If R and S factorize W and Q is any invertible 3 x 3 matrix, then RQ and Q⁻¹S also factorizes W

$$(\mathbf{R}\mathbf{Q})(\mathbf{Q}^{-1}\mathbf{S}) = \mathbf{R}(\mathbf{Q}\mathbf{Q}^{-1})\mathbf{S} = \mathbf{R}\mathbf{S} = \mathbf{W}$$

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Happily, we can take advantage of the fact that if R and S factorize W and Q is any invertible 3 x 3 matrix, then RQ and Q⁻¹S also factorizes W

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- In particular, we look for a **Q** such that

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and then define new matrices

$$\mathbf{R} = \widetilde{\mathbf{R}}\mathbf{Q}$$
$$\mathbf{S} = \mathbf{Q}^{-1}\widetilde{\mathbf{S}}$$

which will still factorize W, but with the orthonormality constraints on R enforced.

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- Why do we refer to **R** as the motion matrix?
 - The first N rows of **R** can be interpreted as the first rows of the rotation matrices that transform to the camera coordinate systems; the second N rows of **R** can be interpreted as the second rows of these transformations.

$$\boldsymbol{p}_{ij} = \begin{pmatrix} \boldsymbol{x}_{ij} \\ \boldsymbol{y}_{ij} \end{pmatrix} = \mathbf{R}^{2x3} \boldsymbol{P}_j = \begin{pmatrix} \mathbf{i}_i^{\mathrm{T}} \\ \mathbf{j}_i^{\mathrm{T}} \end{pmatrix} \boldsymbol{P}_j$$

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• What about translation?

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- Notice, BTW, that G must be a rotation matrix; otherwise, it would destroy the orthnormality imposed by Q.
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 - The first N rows of **R** can be interpreted as the first rows of the rotation matrices that transform to the camera coordinate systems; the second N rows of **R** can be interpreted as the second rows of these transformations.

$$\boldsymbol{p}_{ij} = \begin{pmatrix} x_{ij} \\ y_{ij} \end{pmatrix} = \mathbf{R}^{2x3} \boldsymbol{P}_j = \begin{pmatrix} \mathbf{i}_i^{\mathrm{T}} \\ \mathbf{j}_i^{\mathrm{T}} \end{pmatrix} \boldsymbol{P}_j$$

- What about translation?
 - The *X*, *Y* components of the translations (i.e., those parallel to the image planes) are captured by the shifts of the centroids that we remove during registration. The *Z* components cannot be recovered under orthographic projection.

3D structure and motion: Approaches

Problem statement

- Given image motion
 - Optical flow-based
 - Finite displacement-based
- Seek to recover
 - 3D motion (translation and rotation)
 - 3D structure (geometric layout of environment)

Finite displacement approach

- Seeks to recover
 - full 3D rotation and translation
 - 3D structure
- Typically used in conjunction with finite displacement image motion estimates.

Infinitesimal approach

- Seeks to recover
 - 3D rotational and translation velocity (temporal derivatives of full rotation and translation)
 - 3D structure
- Typically used in conjunction with optical flow image motion estimates.

3D structure and motion: Motivation

Where we are

- Earlier, we suggested how the motion of a point in the world yields corresponding motion in the image.
 - Subject to differences between the motion field and the optical flow.
- Since then, we have developed methods to recover the image motion in terms of optical flow.
 - Gradient-based
 - Finite displacement-based.
- We also have an approach to recovering structure and motion using finite displacements.



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- We also have an approach to recovering structure and motion using finite displacements.

Where we shall go

- Given
 - Our ability to recover motion in the image in terms of infinitesimals
 - And the fact that the image motion arose from 3D structure and motion in the scene
- We now ask how we can "invert" the process to recover the 3D scene parameters from the image motion, all in terms of infinitesimals..



Plan of attack

- We seek to recover estimates of
 - 3D velocity (rotational and translational)
 - 3D structure (distance, Z)

from image motion

- Optical flow

- We must derive an explicit relationship that relates the variables of interest.
- Then we can exploit this relationship in a recovery process.
- As a point of departure, we have the diagram at the right.
- Now we must be explicit about

$$\frac{d\boldsymbol{p}}{dt} = \frac{d\Pi(\boldsymbol{P})}{dt}$$

- This requires
 - 1. Being precise about 3D structure and motion
 - 2. Deriving their image correlates



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3D motion of a point in the scene

• Given a point $P = (X, Y, Z)^{\mathsf{T}}$ in space



3D motion of a point in the scene

- Given a point $P = (X, Y, Z)^{\mathsf{T}}$ in space
- Its motion to $P' = (X', Y', Z')^{\mathsf{T}}$ can be decomposed into 2 parts



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- 1. Translation about the three coordinate axes

$$\mathbf{T} = (t_x, t_y, t_z)^{\mathsf{T}}$$



3D motion of a point in the scene

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2. Rotation about the three coordinates axes

$$\mathbf{\Omega} = (\omega_x, \omega_y, \omega_z)^{\mathsf{T}}$$



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2. Rotation about the three coordinates axes

$$\mathbf{\Omega} = (\omega_x, \omega_y, \omega_z)^{\mathsf{T}}$$

• We have

$$P' = \mathsf{R}(\Omega)P + \mathsf{T}$$

with

- $R(\Omega)$ the rotation matrix corresponding to Ω



Rotation

• An arbitrary rotation is given as

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \omega_x & -\sin \omega_x \\ 0 & \sin \omega_x & \cos \omega_x \end{pmatrix} \begin{pmatrix} \cos \omega_y & 0 & \sin \omega_y \\ 0 & 1 & 0 \\ -\sin \omega_y & 0 & \cos \omega_y \end{pmatrix} \begin{pmatrix} \cos \omega_z & -\sin \omega_z & 0 \\ \sin \omega_z & \cos \omega_z & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} \cos \omega_{y} \cos \omega_{z} & -\cos \omega_{y} \sin \omega_{z} & \sin \omega_{y} \\ \sin \omega_{x} \sin \omega_{y} \cos \omega_{z} + \cos \omega_{x} \sin \omega_{z} & -\sin \omega_{x} \sin \omega_{y} \sin \omega_{z} + \cos \omega_{x} \cos \omega_{z} & -\sin \omega_{x} \cos \omega_{y} \\ -\cos \omega_{x} \sin \omega_{y} \cos \omega_{z} + \sin \omega_{x} \sin \omega_{z} & \cos \omega_{x} \sin \omega_{y} \sin \omega_{z} + \sin \omega_{x} \cos \omega_{z} & \cos \omega_{x} \cos \omega_{z} \end{pmatrix}$$

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• Since we are dealing with velocity, we take the infinitesimal approximations

$$\cos\theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} - \frac{\theta^6}{6!} + \dots \approx 1$$
$$\sin\theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \frac{\theta^7}{7!} + \dots \approx \theta$$

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• Since we are dealing with velocity, we take the infinitesimal approximations

 $\cos\theta \approx 1$ $\sin\theta \approx \theta$

• So that we have

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & -\omega_x \\ 0 & \omega_x & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & \omega_y \\ 0 & 1 & 0 \\ -\omega_y & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & -\omega_z & 0 \\ \omega_z & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \approx \begin{pmatrix} 1 & -\omega_z & \omega_y \\ \omega_z & 1 & -\omega_x \\ -\omega_y & \omega_x & 1 \end{pmatrix}$$

Now we can explicitly calculate a change in 3D position

• The new position *P*' following infinitesimal rotation and translation of *P* is

$$\mathbf{R}\mathbf{P} + \mathbf{T} = \begin{pmatrix} 1 & -\omega_z & \omega_y \\ \omega_z & 1 & -\omega_x \\ -\omega_y & \omega_x & 1 \end{pmatrix} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} + \begin{pmatrix} t_x \\ t_y \\ t_z \end{pmatrix} = \begin{pmatrix} X - \omega_z Y + \omega_y Z + t_x \\ \omega_z X + Y - \omega_x Z + t_y \\ -\omega_y X + \omega_x Y + Z + t_z \end{pmatrix} = \mathbf{P}'$$

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3D velocity also is at hand

• Since velocity is the infinitesimal change in position with time we have

$$\boldsymbol{P} \cdot \boldsymbol{P}' = \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} - \begin{pmatrix} X - \omega_z Y + \omega_y Z + t_x \\ \omega_z X + Y - \omega_x Z + t_y \\ -\omega_y X + \omega_x Y + Z + t_z \end{pmatrix} = \begin{pmatrix} \omega_z Y - \omega_y Z - t_x \\ -\omega_z X + \omega_x Z - t_y \\ \omega_y X - \omega_x Y - t_z \end{pmatrix} = \boldsymbol{V}$$

with V = (U, V, W) 3D velocity.

Where we stand

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Where we stand



Image correlate of 3D structure and motion

• We seek an expression for

$$\frac{d\mathbf{p}}{dt} = \begin{pmatrix} dx / dt \\ dy / dt \end{pmatrix} = \begin{pmatrix} \dot{x} \\ \dot{y} \end{pmatrix} = \begin{pmatrix} u \\ v \end{pmatrix}$$

where we follow Newton's "dot" convention for a temporal derivative.

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• Let us follow perspective projection with f=1, hence

$$x = \frac{X}{Z} \qquad y = \frac{Y}{Z}$$

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• So, we have

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• As well as

$$\boldsymbol{V} = \begin{pmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{pmatrix} = \begin{pmatrix} \omega_z Y - \omega_y Z - t_x \\ -\omega_z X + \omega_x Z - t_y \\ \omega_y X - \omega_x Y - t_z \end{pmatrix}$$

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• Upon substitution we find that

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = \frac{1}{Z}(\omega_z Y - \omega_y Z - t_x) - \frac{X}{Z^2}(\omega_y X - \omega_x Y - t_z)$$

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• Upon substitution we find that (dividing through by Z and simplifying X/Z, Y/Z, Z/Z)

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = \frac{1}{Z}(\omega_z Y - \omega_y Z - t_x) - \frac{X}{Z^2}(\omega_y X - \omega_x Y - t_z)$$
$$= (\omega_z y - \omega_y - \frac{t_x}{Z}) - \frac{X}{Z}(\omega_y x - \omega_x y - \frac{t_z}{Z})$$

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• Upon substitution we find that (simplifying X/Z)

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = (\omega_z y - \omega_y - \frac{t_x}{Z}) - \frac{X}{Z}(\omega_y x - \omega_x y - \frac{t_z}{Z})$$
$$= (\omega_z y - \omega_y - \frac{t_x}{Z}) - x(\omega_y x - \omega_x y - \frac{t_z}{Z})$$

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• Upon substitution we find that (rearranging)

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = (\omega_z y - \omega_y - \frac{t_x}{Z}) - x(\omega_y x - \omega_x y - \frac{t_z}{Z})$$
$$= \frac{1}{Z}(xt_z - t_x) + \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$

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• Upon substitution we find that (and similarly for v)

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = \frac{1}{Z}(xt_z - t_x) + \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v = \frac{\dot{Y}}{Z} - \frac{Y\dot{Z}}{Z^2} = \frac{1}{Z}(yt_z - t_y) + \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

We have achieved our (interim) goal

- We have an explicit relationship that relates
 - image velocity (u(x,y),v(x,y))
 - 3D parameters of structure, Z(x,y)
 - 3D motion, $(\omega_x \omega_y, \omega_z), (t_x, t_y, t_z)$

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Equations of the Motion field

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Equations of the Motion field

Observations

- The rotation and translation components do not directly interact.
- The structure component interacts directly only with the translation component.
- If we know the 3D motion parameters and have recovered the flow (u,v), then it is trivial to recover Z (modulo noise)
- However, we often have little (or no) knowledge of the 3D motion.
Where we stand

- We have developed methods to recover image motion (optical flow) from a time varying image sequence.
- We have derived an explicit relationship to relate the image motion to the corresponding 3D structure and motion.

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Where we will go

- We seek an approach to the recovery of 3D structure and motion from the estimated image motion.
- In general, this is a very difficult problem.
 - Although approaches have been developed
 - With varying success
- We will consider 2 special cases.
- 1. Recovery of 3D structure, Z(x,y), given motion parameters
- 2. Recovery of 3D rotation, assuming no translation.

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3D structure and motion: 3D structure

We assume that the 3D motion parameters are known

• We have two equations in one unknown!

$$u = \frac{\dot{X}}{Z} - \frac{X\dot{Z}}{Z^2} = \frac{1}{Z}(xt_z - t_x) + \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
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• We "derotate" the optical flow

$$u - \omega_{x}(xy) + \omega_{y}(x^{2} + 1) - \omega_{z}(y) = \frac{1}{Z}(xt_{z} - t_{x})$$
$$v - \omega_{x}(y^{2} + 1) + \omega_{y}(xy) + \omega_{z}(x) = \frac{1}{Z}(yt_{z} - t_{y})$$

3D structure and motion: 3D structure

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• From the derotated flow we can calculate Z, perhaps averaging the two recovered values

$$u - \omega_x(xy) + \omega_y(x^2 + 1) - \omega_z(y) = \frac{1}{Z}(xt_z - t_x)$$
$$v - \omega_x(y^2 + 1) + \omega_y(xy) + \omega_z(x) = \frac{1}{Z}(yt_z - t_y)$$
$$\Rightarrow$$

$$Z(x, y) = \frac{xt_z - t_x}{u - \omega_x(xy) + \omega_y(x^2 + 1) - \omega_z(y)}$$

$$Z(x, y) = \frac{yt_z - t_y}{v - \omega_x(y^2 + 1) + \omega_y(xy) + \omega_z(x)}$$

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We assume purely 3D rotation

• We specialize the general case

$$u = \frac{1}{Z}(xt_z - t_x) + \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v = \frac{1}{Z}(yt_z - t_y) + \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

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$$u = \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
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to

$$u = \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v = \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

Remarks

- We recall that flow due to purely 3D rotation is independent of 3D scene structure.
- We see that given 3 measurements alone, we could recover the rotational velocity
- But this would be naively prone to noise sensitivity
 - So we follow another path.

Error formulation

- We seek rotational parameters that minimize the squared error between
 - The observed flow (u, v)
 - And the supposed parametric model of rotational flow

$$u_{rot} = \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v_{rot} = \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

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 - And the supposed parametric model of rotational flow

$$u_{rot} = \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v_{rot} = \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

• We accumulate this error over the entire image domain, *I*, so that we consider

$$\min_{\omega_x,\omega_y,\omega_z} \iint_I \left[(u - u_{rot})^2 + (v - v_{rot})^2 \right] dxdy$$

Error formulation

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• Differentiation WRT \mathcal{O}_{χ} yields

$$\iint_{I} \left[-2(u-u_{rot})xy - 2(v-v_{rot})(y^{2}+1)\right] dxdy$$

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• Differentiation WRT \mathcal{O}_{y} (and setting to zero) yields

$$\iint_{I} [(u - u_{rot})(x^2 + 1) + (v - v_{rot})xy]dxdy = 0$$

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• We accumulate this error over the entire image domain, *I*, so that we consider

$$\min_{\omega_x,\omega_y,\omega_z} \iint_{I} \left[(u - u_{rot})^2 + (v - v_{rot})^2 \right] dxdy$$

• Differentiation WRT \mathcal{O}_z (and setting to zero) yields

$$\iint_{I} [(u - u_{rot})y - (v - v_{rot})x]dxdy = 0$$

Equation counting

• We have 3 equations in 3 unknowns

$$\iint_{I} [(u - u_{rot})xy + (v - v_{rot})(y^{2} + 1)]dxdy = 0$$

$$\iint_{I} [(u - u_{rot})(x^{2} + 1) + (v - v_{rot})xy]dxdy = 0$$

$$\iint_{I} [(u - u_{rot})y - (v - v_{rot})x]dxdy = 0$$

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$$\iint_{I} [(u - u_{rot})y - (v - v_{rot})x]dxdy = 0$$

• So, we proceed to isolate the rotational parameters of interest

$$\iint_{I} [uxy + v(y^{2} + 1)]dxdy = \iint_{I} [u_{rot}xy + v_{rot}(y^{2} + 1)]dxdy$$
$$\iint_{I} [u(x^{2} + 1) + vxy]dxdy = \iint_{I} [u_{rot}(x^{2} + 1) + v_{rot}xy]dxdy$$
$$\iint_{I} [uy - vx]dxdy = \iint_{I} [u_{rot}y - v_{rot}x]dxdy$$

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• So, we proceed to isolate the rotational parameters of interest

Let's introduce
notation for the
LHS
$$\iint_{I} [uxy + v(y^{2} + 1)] dxdy = \iint_{I} [u_{rot}xy + v_{rot}(y^{2} + 1)] dxdy$$
$$\iint_{I} [u(x^{2} + 1) + vxy] dxdy = \iint_{I} [u_{rot}(x^{2} + 1) + v_{rot}xy] dxdy$$
$$\iint_{I} [uy - vx] dxdy = \iint_{I} [u_{rot}y - v_{rot}x] dxdy$$

Equation counting

• We have 3 equations in 3 unknowns

$$\iint_{I} [(u - u_{rot})xy + (v - v_{rot})(y^{2} + 1)]dxdy = 0$$
$$\iint_{I} [(u - u_{rot})(x^{2} + 1) + (v - v_{rot})xy]dxdy = 0$$
$$\iint_{I} [(u - u_{rot})y - (v - v_{rot})x]dxdy = 0$$

• So, we proceed to isolate the rotational parameters of interest

$$a = \iint_{I} [u_{rot} xy + v_{rot} (y^{2} + 1)] dx dy$$
$$b = \iint_{I} [u_{rot} (x^{2} + 1) + v_{rot} xy] dx dy$$
$$c = \iint_{I} [u_{rot} y - v_{rot} x] dx dy$$

Isolating the rotational parameters

• Let us expand the first equation

$$a = \iint_{I} [u_{rot} xy + v_{rot} (y^2 + 1)] dxdy$$

in terms of

$$u_{rot} = \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
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• We find

$$a = \iint_{I} [\omega_{x}(xy) - \omega_{y}(x^{2} + 1) + \omega_{z}(y)]xy + [\omega_{x}(y^{2} + 1) - \omega_{y}(xy) - \omega_{z}(x)](y^{2} + 1)]dxdy$$

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• Grouping by the rotational parameters yields

$$a = \iint_{I} \omega_{x} [x^{2}y^{2} + (y^{2} + 1)^{2}] - \omega_{y} [xy(x^{2} + y^{2} + 2)] - \omega_{z} [x] dxdy$$

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• Since the rotation is constant over the image domain, we pull $\omega_x, \omega_y, \omega_z$ outside the integrals

$$a = \omega_x \iint x^2 y^2 + (y^2 + 1)^2 dx dy - \omega_y \iint xy(x^2 + y^2 + 2) dx dy - \omega_z \iint x dx dy$$

3 equations in 3 unknowns ready for solution

• For compactness of notation let us write

$$a = \omega_x \iint x^2 y^2 + (y^2 + 1)^2 dx dy - \omega_y \iint xy(x^2 + y^2 + 2) dx dy - \omega_z \iint x dx dy$$

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as
$$a = \omega_x(j) + \omega_y(k) + \omega_z(t)$$

3 equations in **3** unknowns ready for solution

• For compactness of notation let us write

$$a = \omega_x \iint x^2 y^2 + (y^2 + 1)^2 dx dy - \omega_y \iint xy(x^2 + y^2 + 2) dx dy - \omega_z \iint x dx dy$$
as

$$a = \omega_x(j) + \omega_y(k) \quad \omega_z(l)$$

• Similarly, we can derive expressions for the other two constraint equations along the lines of

$$b = \omega_x(m) + \omega_y(n) + \omega_z(o)$$
$$c = \omega_x(p) + \omega_y(q) + \omega_z(r)$$

Matrix formulation

• From

$$a = \omega_x(j) + \omega_y(k) + \omega_z(l)$$
$$b = \omega_x(m) + \omega_y(n) + \omega_z(o)$$
$$c = \omega_x(p) + \omega_y(q) + \omega_z(r)$$

Matrix formulation

• From

$$a = \omega_x(j) + \omega_y(k) + \omega_z(l)$$
$$b = \omega_x(m) + \omega_y(n) + \omega_z(o)$$
$$c = \omega_x(p) + \omega_y(q) + \omega_z(r)$$

• We derive the matrix form

$$\begin{pmatrix} j & k & l \\ m & n & o \\ p & q & r \end{pmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} a \\ b \\ c \end{pmatrix}$$

Solution

• From the matrix form

$$\begin{pmatrix} j & k & l \\ m & n & o \\ p & q & r \end{pmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} a \\ b \\ c \end{pmatrix}$$

Solution

• From the matrix form

$$\begin{pmatrix} j & k & l \\ m & n & o \\ p & q & r \end{pmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} a \\ b \\ c \end{pmatrix}$$

• We have solution via the inverse operation

$$\begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} j & k & l \\ m & n & o \\ p & q & r \end{pmatrix}^{-1} \begin{pmatrix} a \\ b \\ c \end{pmatrix}$$

By the way

• Straightforward calculation yields the coefficient expansions we skimmed over

$$m = -k$$

$$n = -\iint (x^{2} + 1)^{2} + x^{2} y^{2} dx dy$$

$$o = \iint y dx dy$$

$$p = l$$

$$q = -o$$

$$r = \iint x^{2} + y^{2} dx dy$$

Where we stand

- We have developed methods to recover image motion (optical flow) from a time varying image sequence.
- We have derived an explicit relationship to relate the image motion to the corresponding 3D structure and motion.

Where we will go

- We seek an approach to the recovery of 3D structure and motion from the estimated image motion.
- In general, this is a very difficult problem.
 - Although approach have been developed
 - With varying success
- We will consider 2 special cases.
- 1. Recovery of 3D structure, Z(x,y), given motion parameters
- 2. Recovery of 3D rotation, assuming no translation.

- In a similar spirit we could attack
 - The pure translation case
 - The general case (unknown structure, rotation and translation)

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We assume purely 3D translation

• We specialize the general case

$$u = \frac{1}{Z}(xt_z - t_x) + \omega_x(xy) - \omega_y(x^2 + 1) + \omega_z(y)$$
$$v = \frac{1}{Z}(yt_z - t_y) + \omega_x(y^2 + 1) - \omega_y(xy) - \omega_z(x)$$

to

$$u = \frac{1}{Z}(xt_z - t_x)$$
$$v = \frac{1}{Z}(yt_z - t_y)$$

Remarks

- We recall that flow due to purely 3D translation is intertwined with 3D scene structure. is independent of 3D scene structure.
- Z varies (potentially) with each image location.
- Translation parameters are constant across the image.
- Notice the scale ambiguity between scene structure, Z, and translation, (t_x, t_y, t_z)
3D structure and motion: 3D translation

Error formulation

- We seek scene structure and translation parameters that minimize the squared error between
 - The observed flow (u, v)
 - And the supposed parametric model of translational flow

$$u_{trans} = \frac{1}{Z} (xt_z - t_x)$$
$$v_{trans} = \frac{1}{Z} (yt_z - t_y)$$

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• We accumulate this error over the entire image domain, *I*, so that we consider

$$\min_{t_x,t_y,t_z,Z} \iint_I \left[(u - u_{trans})^2 + (v - v_{trans})^2 \right] dxdy$$

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- A solution can be had by pursuing a path analogous to that followed for recovery of rotational parameters.
- A new wrinkle is in the apparent need to decouple the translation and scene structure; various approaches have been developed, including
 - Iterating between recovering translation and structure, while holding the other constant.
 - Initially eliminating Z and solving for (t_x, t_y, t_z) and subsequently recovering Z. 111

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We assume no more than instantaneous motion

• We have our general case

$$u = \frac{1}{Z}(xt_{z} - t_{x}) + \omega_{x}(xy) - \omega_{y}(x^{2} + 1) + \omega_{z}(y)$$
$$v = \frac{1}{Z}(yt_{z} - t_{y}) + \omega_{x}(y^{2} + 1) - \omega_{y}(xy) - \omega_{z}(x)$$

and make no specializations.

Error formulation

- We seek scene structure, translational and rotational parameters that minimize the squared error between
 - The observed flow (u, v)
 - And the supposed parametric model of the general visual motion field

$$u_{gen} = \frac{1}{Z} (xt_z - t_x) + \omega_x (xy) - \omega_y (x^2 + 1) + \omega_z (y)$$
$$v_{gen} = \frac{1}{Z} (yt_z - t_y) + \omega_x (y^2 + 1) - \omega_y (xy) - \omega_z (x)$$

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• We accumulate this error over the entire image domain, *I*, so that we consider

$$\min_{t_x,t_y,t_z,\omega_x,\omega_y,\omega_z,Z} \iint_{I} [(u-u_{gen})^2 + (v-v_{rot})^2] dx dy$$

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$$\min_{t_x,t_y,t_z,\omega_x,\omega_y,\omega_z,Z} \iint_{I} \left[(u - u_{gen})^2 + (v - v_{gen})^2 \right] dxdy$$

• Again, analogous methods to those used so far can be brought to bear to yield a solution.

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Remark

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But, instead of developing the details we look at some empirical results derived from a general solution.

Empirical examples presented in lecture.

3D structure and motion: Final remarks

Flow-based

- Works with minimal number of frames (n=2).
- Assumes infinitesimal 3D motion and full perspective projection.
- Provides dense 3D distance estimates.
- Can be numerically sensitive

Factorization-based

- Works with larger temporal streams of frames (n>2).
- Assumes arbitrary 3D motion and orthographic projection (but extensions to more general projection models have been developed).
- Provides 3D shape estimates only at tracked feature points.
- Reasonably numerically stable; at least for orthographic cases...

Summary

- Motion field vs. optical flow
- Brightness constancy
- Gradient-based optical flow estimation
- Finite displacement and feature-based methods
- 3D Structure and motion